INTRODUCTION

Dry powdered polymers (DPP) can be used as stabilising binder for the construction or rehabilitation of granular pavements. Polymer stabilising binders have the effect of waterproofing materials which otherwise would lose significant strength if subjected to moisture ingress. These notes provide guidance for evaluating the suitability of DPP as a stabilising binder and outlines application and construction methods.

Unlike other stabilising binders that contain fly ash/lime mixtures, DPP stabilisation does not result in the development of strong cementitious bonds. Shrinkage cracking or brittle fatigue of the stabilised pavement is unlikely to occur and the pavement functions as a flexible, low permeability protective barrier to the subgrade.

DRY POWDERED POLYMER STABILISATION

DPP is a road stabilising binder consisting of an insoluble polymer that is thermally bound to a very fine carrier such as fly ash. The product, when mixed with hydrated lime has the effect of flocculating and coating clay particles within the pavement material. The fly ash, which is encapsulated by the polymer, is effectively inert and does not react chemically in the stabilisation process. Its only function is to facilitate the distribution of the polymer throughout the pavement material.

Polymers act to preserve the dry strength of pavement materials by creating a hydrophobic soil matrix reducing permeability and minimising water absorption into the clayey fines.

Two DPP products are commercially available:

- A blend of 2:1 polymer-coated fly ash/hydrated lime;
- A blend of 1:1 polymer-coated fly ash/hydrated lime.

The latter product is recommended for use with higher plasticity materials with a PI in excess of 12 but less than 20. Most pavement base materials in Victoria have a PI less than 12 so the 2:1 blend is most commonly used.

Laboratory testing of marginal quality gravel, granitic sand, soft rock and ripped rock (PI range 5 to 7) stabilised with 2:1 blend has indicated the following to varying degrees:

- A reduction in capillary rise and water absorption;
- An increase in the CBR with the lower strength materials showing the greater increase;
- An increase in resilient modulus (increase in stiffness);
- A decrease in permanent deformation (more rut resistant).

The improvement to natural gravels and sands was more pronounced that for soft rock or ripped rock.

The use of DPP stabilising binder should not be expected to make up for inadequate pavement thickness or gross deficiencies in grading, cohesion or aggregate ‘soundness’. Poorly graded and non-cohesive materials may require correction by addition of another granular material as part of the stabilisation work.

SPREADING RATES

The selection of DPP product type is based on the plasticity index (PI) of the material to be stabilised. For highly plastic materials PI > 20, the lime content of the blend may need to be increased to reduce the plasticity of the material to a PI < 8.

Typical spreading rates are in the range of 1.5 to 2% by mass of treated material.

Laboratory testing has indicated that the ability of DPP to resist the ingress of water can be variable with coarse-grained permeable gravels requiring a higher spreading rate.

TESTING FOR SUITABILITY

To determine the suitability of DPP for the stabilisation of a granular pavement material, tests such as plasticity index, grading, maximum dry density and optimum moisture content should be undertaken.

To assess the water-proofing effect of the DPP on the stabilised material, AS 1141.53 – Absorption, swell and capillary rise of compacted materials, is used. For stabilised materials, a capillary rise of 25% (max) over a 24 hour period is recommended and the sample should exhibit no swell under the test conditions. For comparison, an untreated sample should also be prepared and tested.
If, after testing, it is found that the nominated type and quantity of DPP does not produce a material conforming to the specified limit, then an increased dosage rate or an alternative binder should be evaluated by further testing.

If required, testing for stiffness and deformation can be undertaken using the Repeated Load Triaxial Test (RLT) of treated and untreated test specimens. This test has been found to clearly show whether or not DPP stabilisation will produce a significant improvement in the performance of the material.

**PAVEMENT DESIGN CONSIDERATIONS**

Stabilisation with DDP will, to varying degrees:

- Reduce susceptibility to moisture;
- Preserve the dry strength of plastic materials when wetted up;
- Produce a flexible base course layer with low permeability resulting in increased pavement life;
- Provide a strong cohesive surface for a sprayed seal treatment.

Pavement thickness is determined in exactly the same manner as for unbound flexible pavements.

RLT testing and layered elastic analysis can be used to evaluate the relative effects of using treated and untreated materials on the predicted pavement life.

**USE IN PAVEMENT REHABILITATION**

Stabilisation of pavement materials with DDP has been used successfully for major patching rehabilitation of pavements constructed from marginal materials such as granitic sands and natural gravels particularly those with a high degree of moisture sensitivity. The surface of the stabilised layer is relatively resistant to abrasion and may be left unsurfaced for several days without excessive raveling.

It has been found that full width stabilisation of the pavement (i.e. including the shoulders) is desirable to reduce ‘edge effect’ cracking at the shoulder/pavement interface. It is also reported that re-growth of weeds is suppressed on treated shoulders.

**CONSTRUCTION PROCEDURES**

Pavement construction is carried out using the same specialised plant and equipment to that used for pavements stabilised with cementitious binders. DPP can be delivered either in 20 kg bags for small patches carried out as a routine maintenance activity or in bulk pneumatic tankers for larger rehabilitation or construction works.

It is essential that the DPP binder is uniformly mixed throughout the full depth of stabilisation. To achieve this, two mixing runs are recommended.

When treating highly plastic materials, it is advantageous to pre-treat the material with lime to reduce the plasticity of the material to an acceptable level prior to the addition of DPP.

To achieve optimum moisture content (OMC), water is best incorporated during the first mixing run. In practice, it has been found most important that the DDP stabilised layer is compacted at 1 to 2% dry of the OMC of the untreated material. As the hydrophobic effect of the additive repels moisture it is good practice to compact as close as practical behind the mixer before the material becomes too dry.

Unlike cementitiously stabilised materials with a confined working time, there is no such restriction on the working time for a material stabilised with DPP. It may also be remixed, reshaped or re-compacted without loss of dry strength.

**REFERENCES**


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